# SCE 594: Special Topics in Intelligent Automation & Robotics

Lecture 10: Rigid body dynamics II & MAV dynamics



- Recap last lectures
- Covector nature of wrenches and momenta
- Rigid body dynamics
- Case study: Multi-rotor aerial vehicles (MAVs)

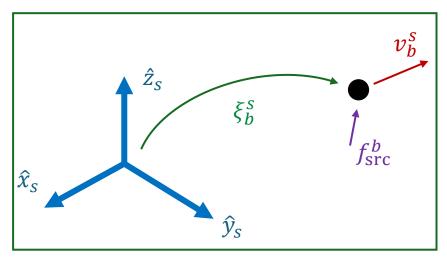


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## Recap: Dynamic modeling

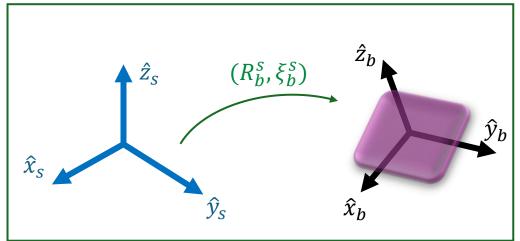
- A dynamic model describes the motion of a system while considering the forces and torques that cause the motion.
- It includes both kinematics and conservation laws



**Forces** on translating point mass

 $\hat{z}_b$   $\hat{z}_s$   $\hat{z}_s$   $\hat{z}_s$   $\hat{z}_s$   $\hat{y}_b$   $\hat{y}_s$ 

Torques on rotating rigid body



Wrenches on moving rigid body

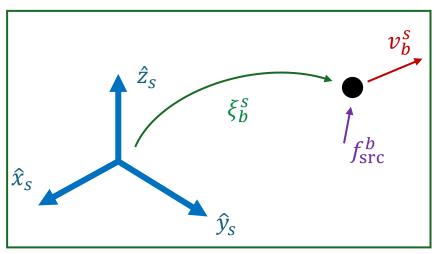


#### Recap: Point mass dynamics

- We will denote by:
  - $f_{\text{src}}^b \in \mathbb{R}^3$ : the abstract force from source src acting on point mass b
  - $f_{\text{src}}^{s,b} \in \mathbb{R}^3$ : the force from source src acting on point mass b, expressed in  $\{s\}$ .
- The kinetic energy of point b,  $E_k: \mathbb{R}^3 \to \mathbb{R}$  is given by:
  - $E_k(v_b^{S,S}) = \frac{1}{2} \operatorname{m}(v_b^{S,S})^{\mathsf{T}} v_b^{S,S}$
- The linear momentum of point b expressed in  $\{s\}$ ,  $P_v^{s,b} \in \mathbb{R}^3$  is given by:
  - $P_v^{s,b} \coloneqq \frac{\partial E_k}{\partial v_b^{s,s}} (v_b^{s,s}) = \mathbf{m} v_b^{s,s}$
- Newton's law:
  - $\dot{P}_{v}^{s,b} = f_{\text{tot}}^{s,b}$

or

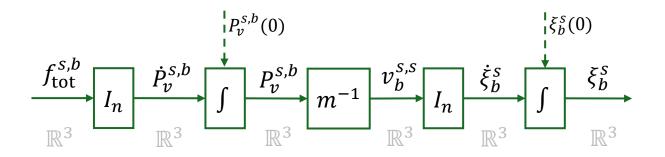
• 
$$\dot{v}_b^{S,S} = \frac{1}{m} f_{\text{tot}}^{S,b}$$





## Recap: Point mass dynamics

In summary,



- $\dot{\xi}_{b}^{s} = v_{b}^{s,s}$   $\dot{P}_{v}^{s,b} = f_{\text{tot}}^{s,b}$

Kinematic relation

Momentum balance

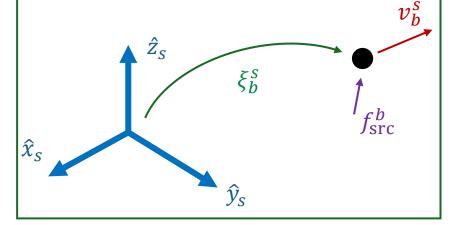
Constitutive relation

Rewritten as

Rewritten as

- $\dot{\xi}_{b}^{s} = v_{b}^{s,s}$   $\dot{v}_{b}^{s,s} = m^{-1} f_{\text{tot}}^{s,b}$

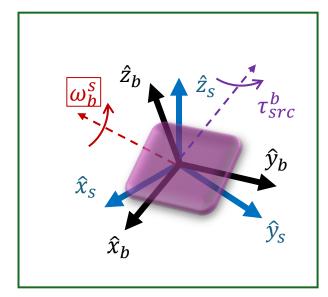
 $\ddot{\xi}_b^s = m^{-1} f_{\text{tot}}^{s,b}$ 



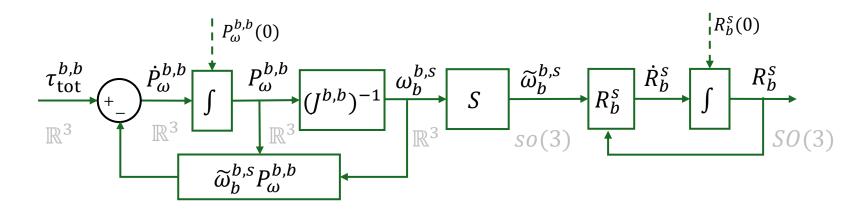


**Forces** on translating point mass

- We will denote by:
  - $\tau_{\rm src}^b \in \mathbb{R}^3$ : the abstract torque from source src acting on body attached to  $\{b\}$
  - $\tau_{\text{src}}^{*,b} \in \mathbb{R}^3$ : the torque from source src acting on body attached to  $\{b\}$ , expressed in  $\{*\}$ .
- The kinetic energy of the rigid body,  $E_k: SO(3) \times \mathbb{R}^3 \to \mathbb{R}$  is given by:
  - $E_k(R_b^s, \omega_b^{*,s}) = \frac{1}{2} (\omega_b^{*,s})^{\mathsf{T}} J^{*,b}(R_b^s) \omega_b^{*,s}$
- The angular momentum of the rigid body expressed in  $\{*\}$ ,  $P_{\omega}^{*,b} \in \mathbb{R}^3$  is given by:
  - $P_{\omega}^{*,b} := \frac{\partial E_k}{\partial \omega_b^{*,s}} \left( R_b^s, \omega_b^{*,s} \right) = J^{*,b} \left( R_b^s \right) \omega_b^{*,s}$
- Euler's law in {s}:
  - $\dot{P}^{s,b}_{\omega} = \tau^{s,b}_{\mathrm{tot}}$







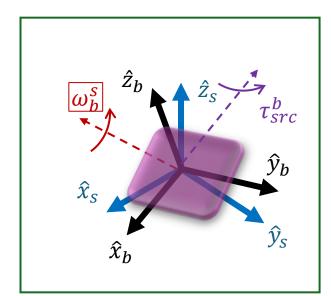
Kinematic relation

Momentum balance

Constitutive relation

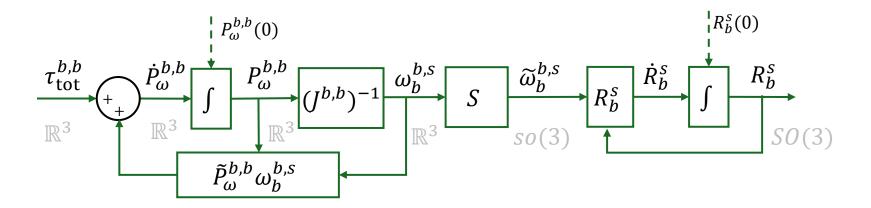
Rewritten as

- $\dot{R}_{b}^{s} = R_{b}^{s} \widetilde{\omega}_{b}^{b,s}$   $\dot{P}_{\omega}^{b,b} = \tau_{\text{tot}}^{b,b} \widetilde{\omega}_{b}^{b,s} P_{\omega}^{b,b}$   $\omega_{b}^{b,s} = (J^{b,b})^{-1} P_{\omega}^{b,b}$





 $P_{\omega}^{*,b} \in \mathbb{R}^3$  is the angular momentum of body attached to  $\{b\}$  expressed in  $\{*\}$  $J^{*,b} \in \mathbb{R}^{3\times 3}$  is the moment of inertia of body attached to  $\{b\}$  expressed in  $\{*\}$ 



Kinematic relation

Momentum balance

Constitutive relation

Or rewritten as

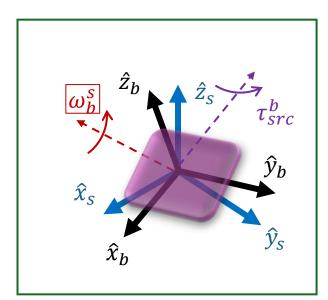
• 
$$\dot{R}_b^s = R_b^s \widetilde{\omega}_b^{b,s}$$

$$\dot{R}_{b}^{S} = R_{b}^{S} \widetilde{\omega}_{b}^{b,S}$$

$$\dot{P}_{\omega}^{b,b} = \tau_{\text{tot}}^{b,b} + \tilde{P}_{\omega}^{b,b} \omega_{b}^{b,S}$$

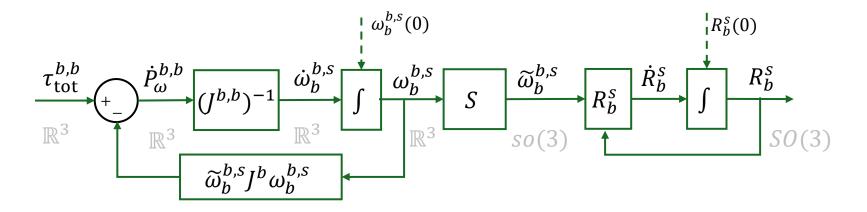
$$\omega_{b}^{b,S} = (J^{b,b})^{-1} P_{\omega}^{b,b}$$

• 
$$\omega_b^{b,s} = (J^{b,b})^{-1} P_\omega^{b,b}$$





 $P_{\omega}^{*,b} \in \mathbb{R}^3$  is the angular momentum of body attached to  $\{b\}$  expressed in  $\{*\}$  $J^{*,b} \in \mathbb{R}^{3\times 3}$  is the moment of inertia of body attached to  $\{b\}$  expressed in  $\{*\}$ 



- $\dot{R}_b^s = R_b^s \widetilde{\omega}_b^{b,s}$
- $\dot{P}^{s,b}_{\omega} = \tau^{s,b}_{\text{tot}}$
- $\omega_h^{b,s} = (J^{b,b})^{-1} P_{\omega}^{b,k}$

Kinematic relation

Momentum balance

Constitutive relation

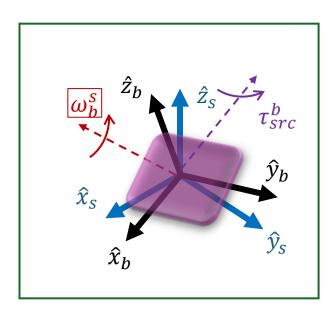
Which can also be written as

$$\dot{R}_b^s = R_b^s \widetilde{\omega}_b^{b,s}$$

$$\dot{\omega}_b^{b,s} = \left(J^{b,b}\right)^{-1} \left(\tau_{\text{tot}}^{b,b} - \widetilde{\omega}_b^{b,s} J^b \omega_b^{b,s}\right)$$



 $P_{\omega}^{*,b} \in \mathbb{R}^3$  is the angular momentum of body attached to  $\{b\}$  expressed in  $\{*\}$   $J^{*,b} \in \mathbb{R}^{3\times 3}$  is the moment of inertia of body attached to  $\{b\}$  expressed in  $\{*\}$ 

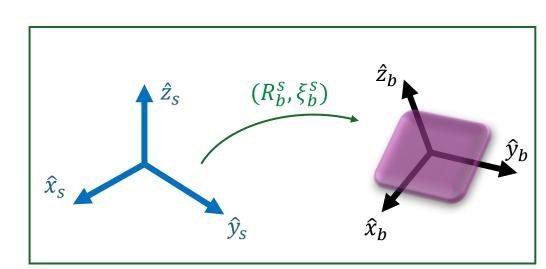


**Torques** on rotating rigid body

- We will denote by:
  - $\mathcal{W}_{\rm src}^b \in (\mathbb{R}^6)^*$ : the abstract wrench from source src acting on body attached to  $\{b\}$
  - $\mathcal{W}_{\text{src}}^{*,b} \in (\mathbb{R}^6)^*$ : the wrench from source src acting on body attached to  $\{b\}$ , expressed in  $\{*\}$ .
- The kinetic energy of the rigid body,  $E_k: SE(3) \times \mathbb{R}^6 \to \mathbb{R}$  is given by:
  - $E_k(H_b^s, \mathcal{V}_b^{*,s}) = \frac{1}{2} (\mathcal{V}_b^{*,s})^{\mathsf{T}} \mathfrak{T}^{*,b} (H_b^s) \mathcal{V}_b^{*,s}$
- The generalized momentum of the rigid body expressed in  $\{*\}$ ,  $P^{*,b} \in (\mathbb{R}^6)^*$  is given by:
  - $P^{*,b} := \frac{\partial E_k}{\partial \mathcal{V}_b^{*,s}} (H_b^s, \mathcal{V}_b^{*,s}) = \mathfrak{T}^{*,b} (H_b^s) \mathcal{V}_b^{*,s}$
- Netwon-Euler's law in {s}:
  - $\dot{P}^{s,b} = \mathcal{W}_{\text{tot}}^{s,b}$



#### Note:



- Recap last lectures
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## Kinetic energy invariance

Kinetic energy is a scalar, so it is a coordinate-free concept.

$$E_k(H_b^s, \mathcal{V}_b^{b,s}) = E_k(H_b^s, \mathcal{V}_b^{s,s}) = E_k(H_b^s, \mathcal{V}_b^{*,s})$$

• Let's examine the kinetic energy of the twist in  $\{b\}$ :

$$E_k(H_b^s, \mathcal{V}_b^{b,s}) = E_k(\mathcal{V}_b^{b,s}) = \frac{1}{2} \left( \mathcal{V}_b^{b,s} \right)^{\mathsf{T}} \mathfrak{T}^{b,b} \, \mathcal{V}_b^{b,s}$$

$$\mathfrak{T}^{b,b} = \begin{pmatrix} J^{b,b} & m \, \tilde{\xi}^b_{\rm cm} \\ -m \tilde{\xi}^b_{\rm cm} & m \, I_3 \end{pmatrix}$$

Generalized inertia



## Kinetic energy invariance

Kinetic energy is a scalar, so it is a coordinate-free concept.

$$E_k(H_b^s, \mathcal{V}_b^{b,s}) = E_k(H_b^s, \mathcal{V}_b^{s,s}) = E_k(H_b^s, \mathcal{V}_b^{*,s})$$

• Let's examine the kinetic energy of the twist in {*b*}:

$$E_k(H_b^s, \mathcal{V}_b^{b,s}) = E_k(\mathcal{V}_b^{b,s}) = \frac{1}{2} \left( \mathcal{V}_b^{b,s} \right)^{\mathsf{T}} \mathfrak{T}^{b,b} \mathcal{V}_b^{b,s}$$

• Using the definition of the generalized momentum, we have that

$$2E_k = \left(\mathcal{V}_b^{b,s}\right)^{\mathsf{T}} P^{b,b} = \left(P^{b,b}\right)^{\mathsf{T}} \mathcal{V}_b^{b,s}$$

$$\mathfrak{T}^{b,b} = \begin{pmatrix} J^{b,b} & m \, \tilde{\xi}^b_{\rm cm} \\ -m \tilde{\xi}^b_{\rm cm} & m \, I_3 \end{pmatrix}$$

Generalized inertia



#### Generalized momentum

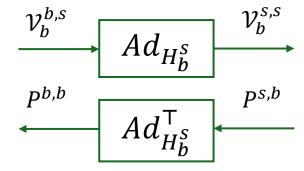
 Due to the invariance of kinetic energy, if we express the momentum and twist in the {s} frame we have that:

$$2E_{k} = (P^{b,b})^{\mathsf{T}} \mathcal{V}_{b}^{b,s} = (P^{b,b})^{\mathsf{T}} A d_{H_{s}^{b}} \mathcal{V}_{b}^{s,s} = (A d_{H_{s}^{b}}^{\mathsf{T}} P^{b,b})^{\mathsf{T}} \mathcal{V}_{b}^{s,s} = (P^{s,b})^{\mathsf{T}} \mathcal{V}_{b}^{s,s}$$

Therefore,

$$|\mathcal{V}_b^{S,S} = Ad_{H_b^S} \mathcal{V}_b^{b,S} \in \mathbb{R}^6$$

$$P^{s,b} = Ad_{H_b^s}^{-\mathsf{T}} P^{b,b} \in (\mathbb{R}^6)^*$$
 Covector





#### Wrench

 Just as with twists, we can merge torques and forces into a six-dimensional object we shall call a wrench.

$$\mathcal{W}^{*,b} = \begin{pmatrix} \tau^{*,b} \\ f^{*,b} \end{pmatrix} \in (\mathbb{R}^6)^*$$

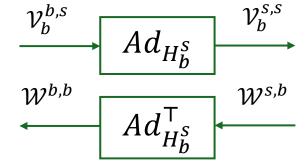
The duality pairing of a wrench and a twists gives mechanical power:

Power = 
$$(\mathcal{W}^{*,b})^{\mathsf{T}} \mathcal{V}_b^{*,s}$$

• Since power is also a coordinate-free concept, we have that

$$| \mathcal{V}_b^{s,s} = Ad_{H_b^s} \mathcal{V}_b^{b,s} \in \mathbb{R}^6$$

$$\mathcal{W}^{s,b} = Ad_{H_b^s}^{-\mathsf{T}} \mathcal{W}^{b,b} \in (\mathbb{R}^6)^*$$
 Covector

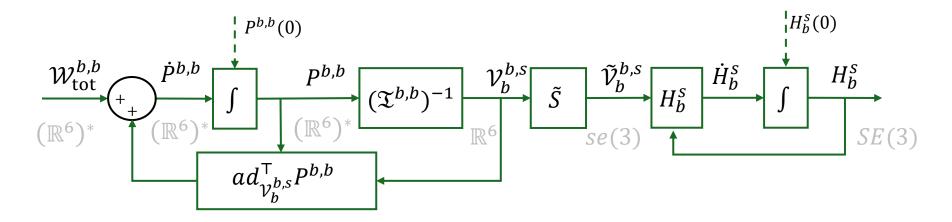




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## Rigid body dynamics

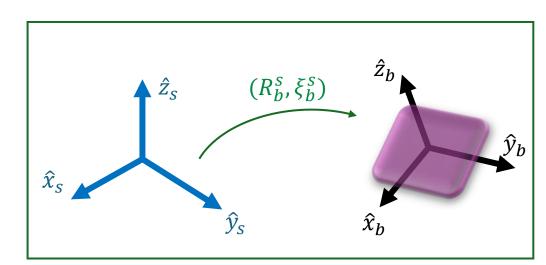


- $\dot{H}_b^S = H_b^S \tilde{\mathcal{V}}_b^{b,S}$   $\dot{P}^{S,b} = \mathcal{W}_{\text{tot}}^{S,b}$   $\mathcal{V}_b^{b,S} = (\mathfrak{T}^{b,b})^{-1} P^{b,b}$

Kinematic relation

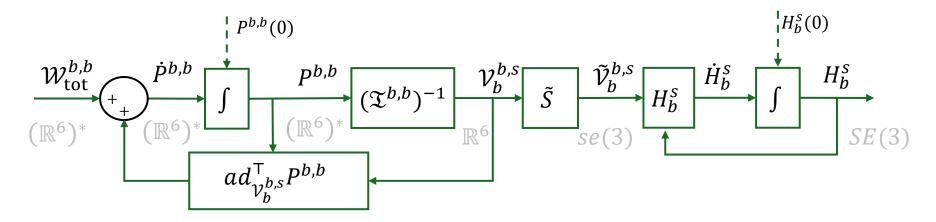
Momentum balance

Constitutive relation





## Rigid body dynamics



- $\dot{H}_b^s = H_b^s \tilde{\mathcal{V}}_b^{b,s}$   $\dot{P}^{s,b} = \mathcal{W}_{\text{tot}}^{s,b}$
- $\mathcal{V}_{b}^{b,s} = (\mathfrak{T}^{b,b})^{-1} P^{b,b}$

Kinematic relation

Momentum balance

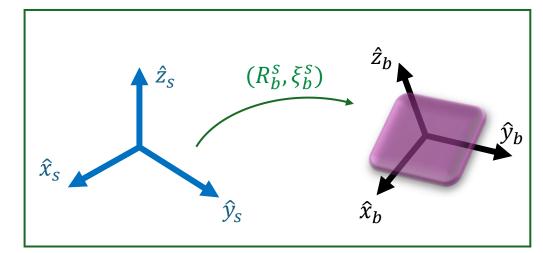
Constitutive relation

Rewritten as

- $\dot{H}_b^s = H_b^s \tilde{\mathcal{V}}_b^{b,s}$
- $\dot{P}^{b,b} = \mathcal{W}_{\text{tot}}^{s,b} + ad_{\mathcal{V}_b^{b,s}}^{\mathsf{T}} P^{b,b}$   $\dot{\mathcal{V}}_b^{b,s} = (\mathfrak{T}^{b,b})^{-1} P^{b,b}$

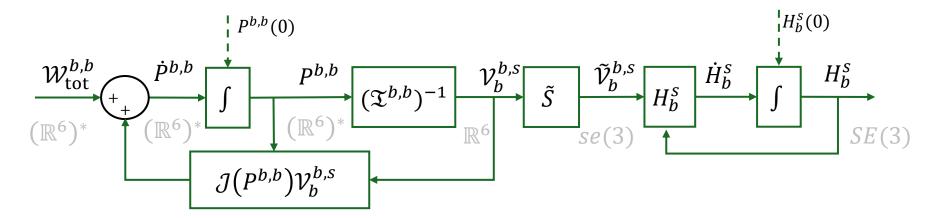
 $ad_{\mathcal{V}_{\iota}^{b,s}}: \mathbb{R}^6 \to \mathbb{R}^6$ 

Provided in the homework





## Rigid body dynamics



- $\dot{H}_b^s = H_b^s \tilde{\mathcal{V}}_b^{b,s}$
- $\dot{P}^{s,b} = \mathcal{W}_{tot}^{s,b}$
- $\mathcal{V}_{b}^{b,s} = (\mathfrak{T}^{b,b})^{-1} P^{b,b}$

Kinematic relation

Momentum balance

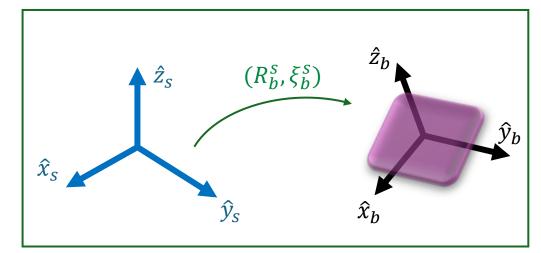
Constitutive relation

Or rewritten as

- $\dot{H}_b^s = H_b^s \tilde{\mathcal{V}}_b^{b,s}$   $\dot{P}^{b,b} = \mathcal{W}_{\text{tot}}^{s,b} + \mathcal{J}(P^{b,b}) \mathcal{V}_b^{b,s}$
- $\mathcal{V}_{h}^{b,s} = (\mathfrak{T}^{b,b})^{-1} P^{b,b}$

 $\mathcal{J}(P^{b,b}): \mathbb{R}^6 \to \mathbb{R}^6$ 

Provided in the homework





- Recap last lectures
- Covector nature of wrenches and momenta
- Rigid body dynamics
- Case study: Multi-rotor aerial vehicles



#### Multi-rotor aerial vehicles

- Multi-rotor aerial vehicles (MAVs) are the most popular choice of aerial robotics platform.
- Usually, they have a simple mechanical structure and few moving parts.
- MAVs are usually modeled as a single rigid body floating in space.



















#### Multi-rotor aerial vehicles

• MAVs are classified based on properties of the map between individual rotor thrusts  $\lambda_i$  and the resultant wrench applied on the MAV's body which is used for control.

$$\mathcal{W}_{\text{con}}^{b,b} = \begin{pmatrix} \tau_{\text{con}}^{b,b} \\ f_{\text{con}}^{b,b} \end{pmatrix} = M(t)\lambda$$



















 $\lambda = (\lambda_1, \cdots, \lambda_{N_p}) \in \mathbb{R}^{N_p}$  is the rotors thrust vector and  $N_p$  is the number of propellers on the MAV.