# SCE 594: Special Topics in Intelligent Automation & Robotics

Topic 3: Fixed-base manipulator modeling

Lecture 11: Forward Kinematics



#### Outline

- Motivation
- Exponential coordinates & Exponential map
- Product of Exponentials (PoE) formula
- Examples



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#### Motivation

 In Topic 3, we will be dealing with the kinematic & dynamic modeling fixed-base open chain manipulators.







Fixed-base closed chain

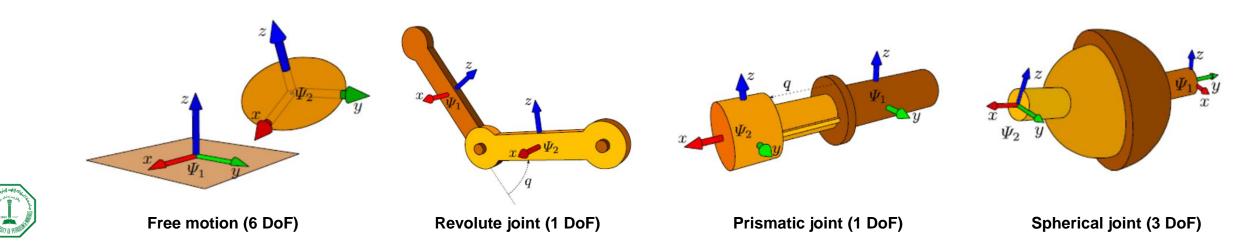


Floating-base open chain

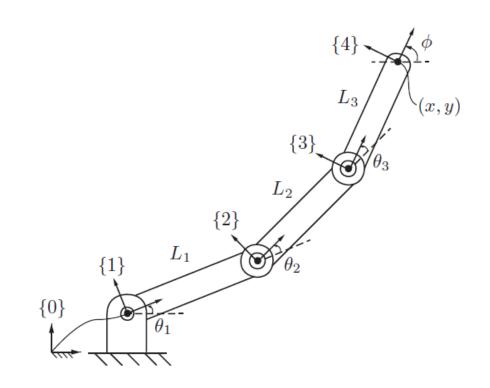


#### Motivation

- Majority of robotic systems can be modeled as several rigid bodies connected by ideal joints.
- An ideal joint (aka kinematic pair) is a purely kinematic relation between two rigid bodies restricting the relative twist  $\mathcal{V}_1^{*,2}$ .
- The degrees of freedom (DoF) of a joint is the number of independent coordinates of  $\mathcal{V}_1^{*,2}$ .



- The forward kinematics of a robot refers to the calculation of the position and orientation of its end-effector frame from its joint coordinates.
- Consider, the 3R planar open chain below.





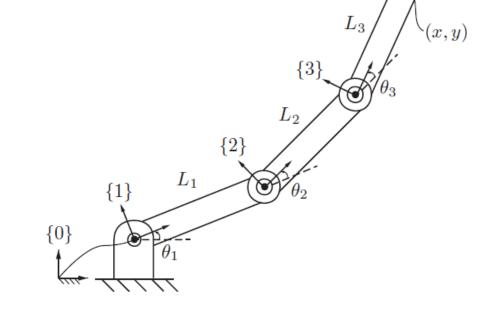
- The forward kinematics of a robot refers to the calculation of the position and orientation of its end-effector frame from its joint coordinates.
- Consider, the 3R planar open chain below.
- The pose of the end-effector's frame {4} is given by:

$$H_4^0 = \begin{pmatrix} c_{\phi} & -s_{\phi} & 0 & x \\ s_{\phi} & c_{\phi} & 0 & y \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$x = L_1 \cos \theta_1 + L_2 \cos(\theta_1 + \theta_2) + L_3 \cos(\theta_1 + \theta_2 + \theta_3),$$
  

$$y = L_1 \sin \theta_1 + L_2 \sin(\theta_1 + \theta_2) + L_3 \sin(\theta_1 + \theta_2 + \theta_3),$$
  

$$\phi = \theta_1 + \theta_2 + \theta_3.$$



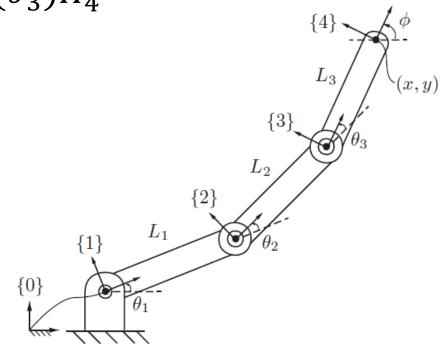


• A systematic way to derive the forward kinematics map  $(\theta_1, \theta_2, \theta_3) \mapsto H_4^0$ 

is to attach a reference frame to each link  $\{1\}$ ,  $\{2\}$ ,  $\{3\}$ .

Then we have that:

$$H_4^0 = H_1^0(\theta_1)H_2^1(\theta_2)H_3^2(\theta_3)H_4^3$$





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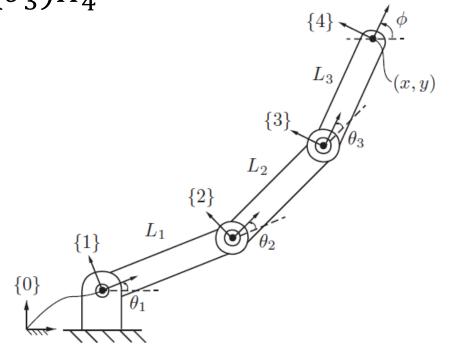
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A widely used convention for choosing thee body-fixed frames {1}, {2}, {3} is based on the so-called Denavit—Hartenberg parameters (D–H parameters). We will use a more powerful approach based on the screw-theory interpretation of twists.





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## Recall linear ODE theory

• Consider the scalar linear ordinary differential equation (ODE):  $\dot{x}(t) = a \; x(t)$ .

where  $x(t) \in \mathbb{R}$  and  $a \in \mathbb{R}$  is a constant.

The solution to the ODE above is given by

$$x(t) = e^{at}x(0),$$

where the exponential function is defined as the series:

$$e^{at} = 1 + at + \frac{(at)^2}{2!} + \frac{(at)^3}{3!} + \cdots$$



## Recall linear ODE theory

Similarly, consider the vector linear ODE:

$$\dot{x}(t) = A x(t),$$

where  $x(t) \in \mathbb{R}^n$  and  $A \in \mathbb{R}^{n \times n}$  is constant.

The solution to the ODE above is given by

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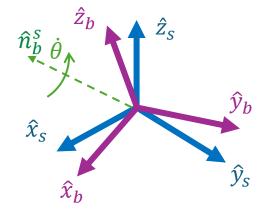
where the matrix exponential function is defined as the series:

$$e^{At} = I + At + \frac{(At)^2}{2!} + \frac{(At)^3}{3!} + \cdots$$



- Suppose that a frame  $\{b\}$  with unit axes  $\{\hat{x}_b, \hat{y}_b, \hat{z}_b\}$  is attached to a rotating body.
- The angular velocity vector describing the instantaneous rotation of  $\{b\}$  relative to  $\{s\}$  is given by  $\omega_b^s \coloneqq \hat{n}_b^s \dot{\theta} \in \mathbb{R}^3$ .
- The instantaneous rate of change of  $R_h^s \in SO(3)$  is given by

$$\dot{R}_b^s = \widetilde{\omega}_b^{s,s} R_b^s$$

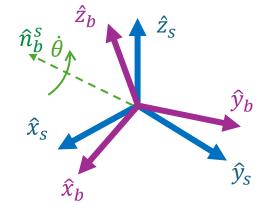




- Assume that  $\omega_b^{s,s}=\hat{n}_b^{s,s}$  is a constant unit vector with  $\dot{\theta}=1$  and thus  $\widetilde{\omega}_b^{s,s}$  is also constant.
- The solution to  $\dot{R}_b^S = \widetilde{\omega}_b^{S,S} R_b^S$  then becomes

$$R_b^s(t) = e^{\tilde{n}_b^{s,s}t} R_b^s(0) \qquad \qquad \tilde{n}_b^{s,s} \coloneqq S(\hat{n}_b^{s,s}) \in so(3)$$

• Intuitively, this is the rotation matrix reached from  $R_b^s(0)$  by rotating it around  $\widehat{\omega}$  at a constant 1 rad/s for t seconds.

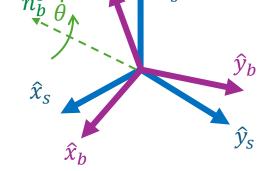




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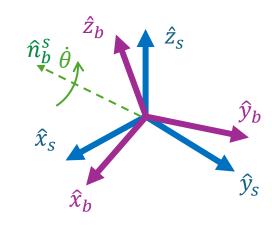
Note that since 
$$\dot{\theta} = 1$$
, we have that  $\theta(t) = \int_0^t \dot{\theta} \ dt = \int_0^t dt = t$ 

• By replacing t with  $\theta$ , we have that

$$R_b^s(\theta) = e^{\tilde{n}_b^{s,s}\theta} R_b^s(0)$$

which is intuitively the rotation matrix achieved by rotating  $R_b^s(0)$  around the axis  $\hat{n}_b^{s,s}$  by an angle  $\theta$ .





# Exponential map of SO(3)

The exponential map

exp: 
$$so(3) \rightarrow SO(3)$$
  
 $\tilde{n}_b^{s,s} \mapsto e^{\tilde{n}_b^{s,s}}$ 

maps elements of the Lie algebra to elements of the Lie group.

- It is surjective, but not injective
  - $\forall R \in SO(3)$ ,  $\exists \tilde{n} \in SO(3)$  s.t.  $R = e^{\tilde{n}}$
  - $\exists \hat{n}_1, \hat{n}_2 \in \mathbb{R}^3$  with  $\hat{n}_1 \neq \hat{n}_2$  s.t.  $e^{\tilde{n}_1} = e^{\tilde{n}_2}$



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Given any pair  $(\hat{n}, \theta) \in \mathbb{S}^2 \times [-\pi, \pi]$ , the matrix exponential  $e^{\tilde{n}\theta} \in SO(3)$  of  $\tilde{n}\theta \in so(3)$ , with  $\tilde{n} \coloneqq S(\hat{n})$ , is given by:

$$e^{\tilde{n}\theta} = I_3 + \sin\theta \, \tilde{n} + (1 - \cos\theta) \tilde{n}^2$$

Rodrigues's formula

# Elementary rotations

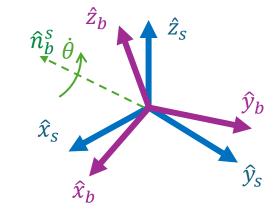
Rotations about the coordinate frame axes are given by:

$$\operatorname{Rot}(\hat{\mathbf{x}}, \theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix},$$

$$\operatorname{Rot}(\hat{\mathbf{y}}, \theta) = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix},$$

$$\operatorname{Rot}(\hat{\mathbf{z}}, \theta) = \begin{bmatrix} \cos \theta & -\sin \theta & 0\\ \sin \theta & \cos \theta & 0\\ 0 & 0 & 1 \end{bmatrix}.$$





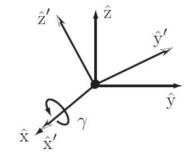
## Roll-Pitch-Yaw Angles

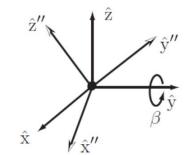
 The roll—pitch—yaw angles refer to the angles in a sequence of rotations about axes fixed in the space frame

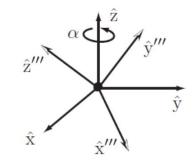
$$R(\alpha, \beta, \gamma) = \operatorname{Rot}(\hat{\mathbf{z}}, \alpha) \operatorname{Rot}(\hat{\mathbf{y}}, \beta) \operatorname{Rot}(\hat{\mathbf{x}}, \gamma) I$$

$$= \begin{bmatrix} \mathbf{c}_{\alpha} & -\mathbf{s}_{\alpha} & \mathbf{0} \\ \mathbf{s}_{\alpha} & \mathbf{c}_{\alpha} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{c}_{\beta} & \mathbf{0} & \mathbf{s}_{\beta} \\ \mathbf{0} & 1 & \mathbf{0} \\ -\mathbf{s}_{\beta} & \mathbf{0} & \mathbf{c}_{\beta} \end{bmatrix} \begin{bmatrix} \mathbf{1} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{c}_{\gamma} & -\mathbf{s}_{\gamma} \\ \mathbf{0} & \mathbf{s}_{\gamma} & \mathbf{c}_{\gamma} \end{bmatrix} I$$

$$= \begin{bmatrix} \mathbf{c}_{\alpha} \mathbf{c}_{\beta} & \mathbf{c}_{\alpha} \mathbf{s}_{\beta} \mathbf{s}_{\gamma} - \mathbf{s}_{\alpha} \mathbf{c}_{\gamma} & \mathbf{c}_{\alpha} \mathbf{s}_{\beta} \mathbf{c}_{\gamma} + \mathbf{s}_{\alpha} \mathbf{s}_{\gamma} \\ \mathbf{s}_{\alpha} \mathbf{c}_{\beta} & \mathbf{s}_{\alpha} \mathbf{s}_{\beta} \mathbf{s}_{\gamma} + \mathbf{c}_{\alpha} \mathbf{c}_{\gamma} & \mathbf{s}_{\alpha} \mathbf{s}_{\beta} \mathbf{c}_{\gamma} - \mathbf{c}_{\alpha} \mathbf{s}_{\gamma} \\ -\mathbf{s}_{\beta} & \mathbf{c}_{\beta} \mathbf{s}_{\gamma} & \mathbf{c}_{\beta} \mathbf{c}_{\gamma} \end{bmatrix}.$$



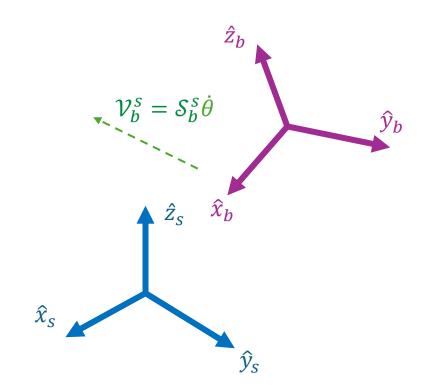






### Screw interpretation of Twists

- Just as an angular velocity  $\omega_b^s$  can be viewed as  $\hat{n}_b^s \dot{\theta} \in \mathbb{R}^3$  where  $\hat{n}_b^s$  is the unit rotation axis and  $\dot{\theta}$  is the rate of rotation about it,
- A twist  $\mathcal{V}_b^s$  can interpreted in terms of a screw axis  $\mathcal{S}_b^s \in \mathbb{R}^6$  and a velocity  $\dot{\theta}$  about the screw axis





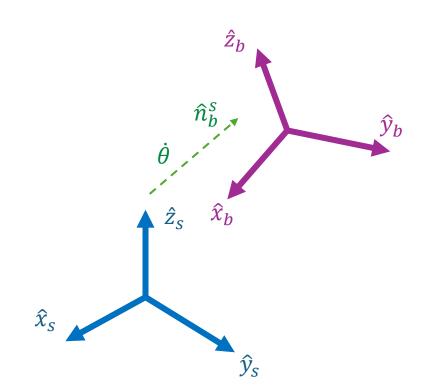
## Screw interpretation of Twists

- We define the screw axis  $\mathcal{S}_b^s$  and  $\dot{\theta}$  in the following manner:
  - a) Pure translation

$$\mathcal{S}_b^s = \begin{pmatrix} 0 \\ \hat{n}_b^s \end{pmatrix} \in \mathbb{R}^6,$$

 $\hat{n}_{h}^{s}$  is the translation axis

 $\dot{\theta}$  is the linear velocity along the screw axis





## Screw interpretation of Twists

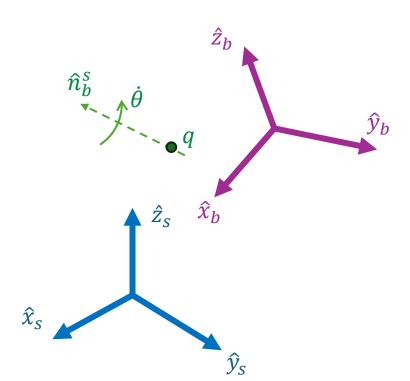
- We define the screw axis  $\mathcal{S}_{b}^{s}$  and  $\dot{\theta}$  in the following manner:
  - b) Pure rotation

$$\mathcal{S}_b^s = \begin{pmatrix} \hat{n}_b^s \\ -\hat{n}_b^s \wedge q \end{pmatrix} \in \mathbb{R}^6,$$

 $\hat{n}_{h}^{s}$  is the rotation axis

 $\dot{\theta}$  is the angular velocity around the screw axis

q is any point on the screw axis



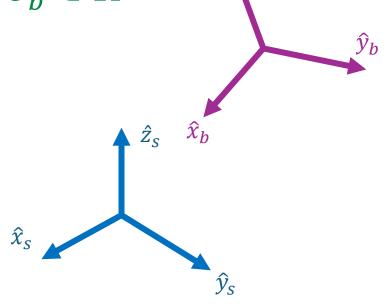


#### Exp. coordinates of homogeneous transformations

• By analogy to the exponential coordinates  $(\hat{n}_b^s, \theta)$  for rotations, we can define the six-dimensional exponential coordinates of a homogeneous transformation  $H_b^s$  by  $\mathcal{S}_b^s \theta \in \mathbb{R}^6$  such that

$$H_b^s(\theta) = e^{\tilde{S}_b^{s,s}\theta} H_b^s(0)$$

where  $\tilde{\mathcal{S}}_b^{s,s} \in se(3)$  is the matrix representation of  $\mathcal{S}_b^s \in \mathbb{R}^6$ 





# Exponential map of SE(3)

The exponential map

exp: 
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maps elements of the Lie algebra to elements of the Lie group.

• It is surjective, but not injective



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