

CIE 482: Path Planning & Navigation for Mobile Robots

Lecture 19: Extended Kalman Filter



Outline

- Recap last lectures
- Extended Kalman Filter Algorithm
- IMU Orientation Estimation



Outline

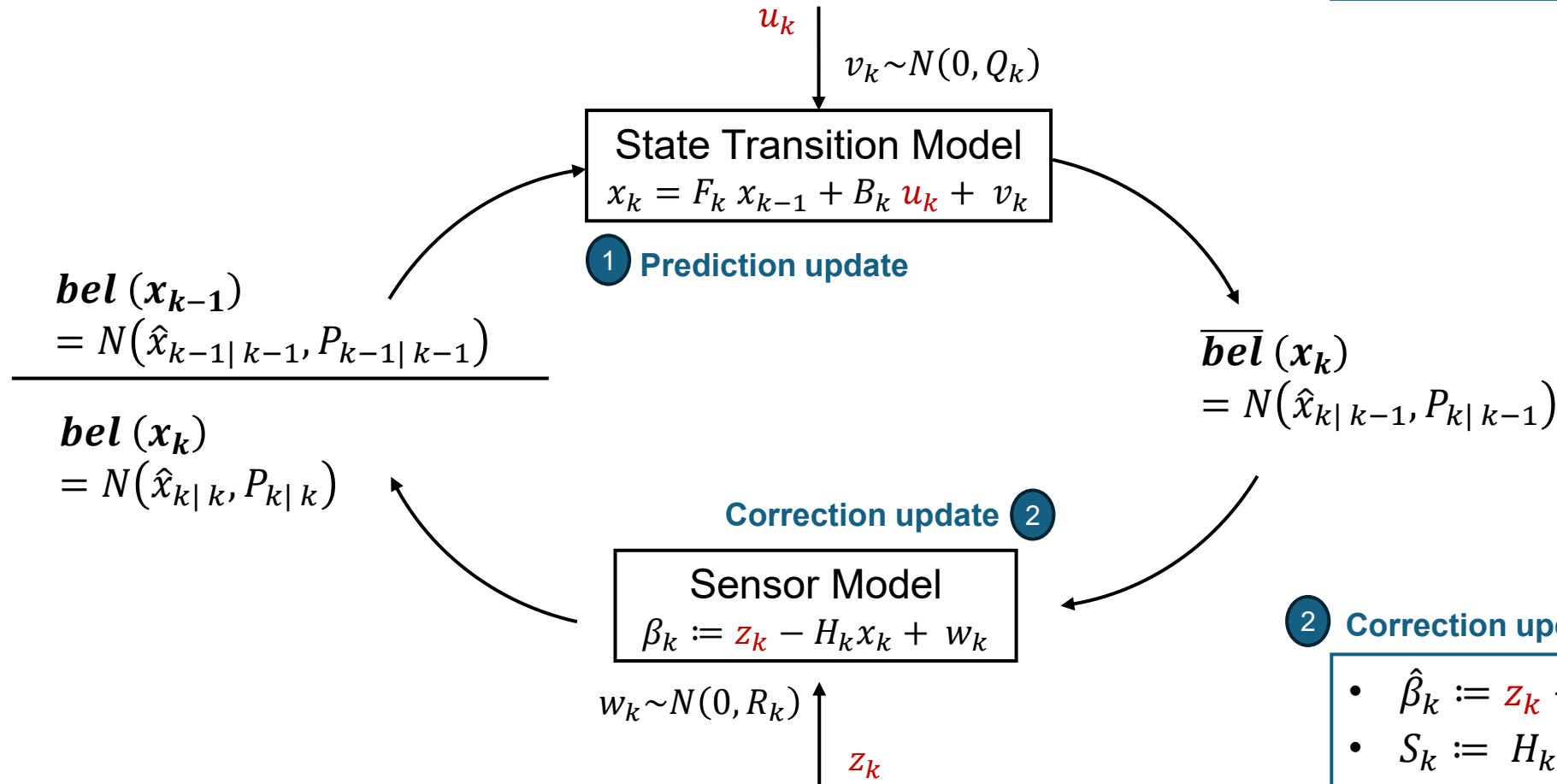
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Kalman Filter Overview

1 Prediction update

- $\hat{x}_{k|k-1} = F_k \hat{x}_{k-1|k-1} + B_k u_k$
- $P_{k|k-1} = F_k P_{k-1|k-1} F_k^\top + Q_k$



1 Prediction update

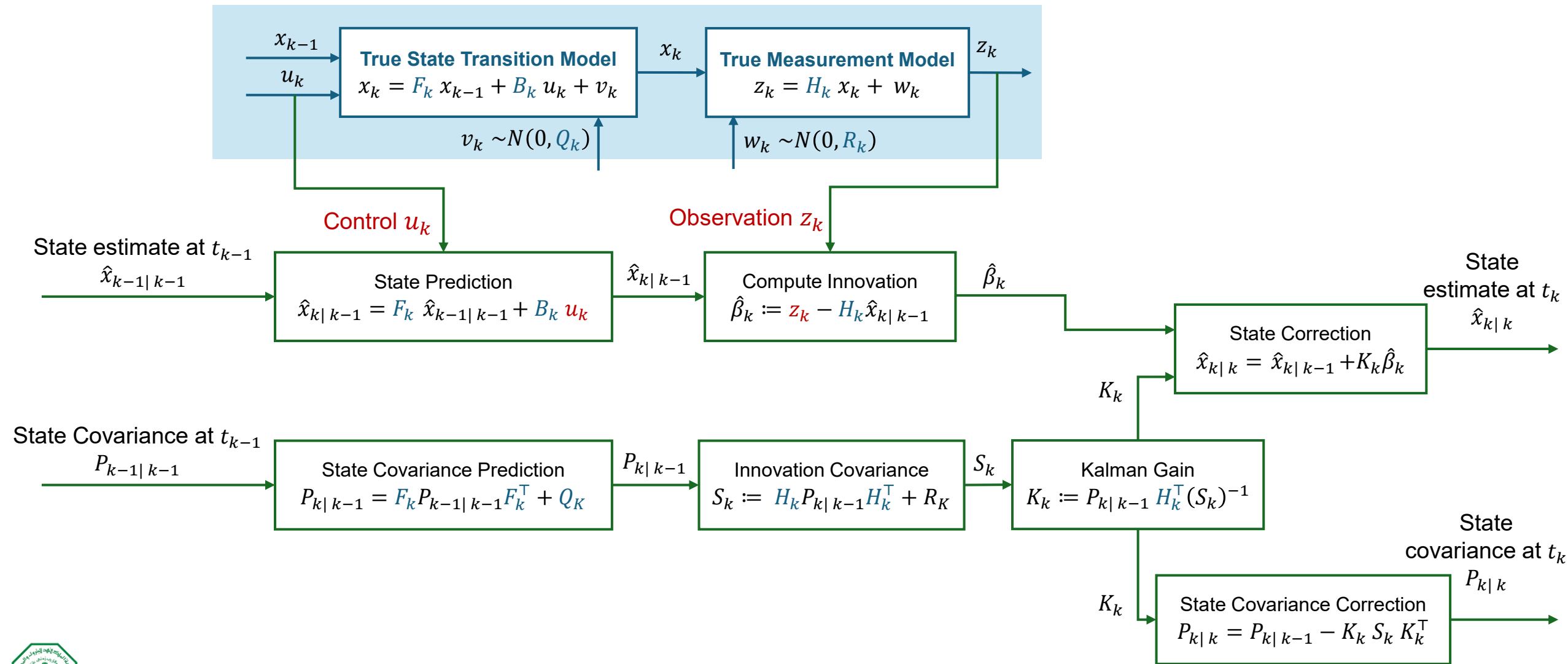
2 Correction update

2 Correction update

- $\hat{\beta}_k := z_k - H_k \hat{x}_{k|k-1}$
- $S_k := H_k P_{k|k-1} H_k^\top + R_k$
- $K_k := P_{k|k-1} H_k^\top (S_k)^{-1}$
- $\hat{x}_{k|k} = \hat{x}_{k|k-1} + K_k \hat{\beta}_k$
- $P_{k|k} = P_{k|k-1} - K_k S_k K_k^\top$



Kalman Filter Block Diagram



Recap: Drawbacks of standard Kalman filter

- KF works well when dynamics and sensors are actually linear.
- Problem:
 - Real-world systems (like mobile robots) often have nonlinear dynamics or nonlinear sensors.
- One of the possible extensions of the Kalman filter to nonlinear systems is the **Extended Kalman Filter (EKF)**.
- The idea behind it is that it **linearizes** the nonlinear models around the latest estimate $\hat{x}_{k-1|k-1}$.



Recall: Taylor series expansion

- Note that this allows us to approximate the function $f(x)$ near the vector $x_0 \in \mathbb{R}^n$ by the linear set of equations:

$$f(x) \approx f(x_0) + J_f(x_0)(x - x_0),$$

$\mathbb{R}^n \qquad \mathbb{R}^{n \times n} \qquad \mathbb{R}^n$

$$f(x) \approx \begin{pmatrix} f_1(x_0) \\ \vdots \\ f_n(x_0) \end{pmatrix} + \begin{pmatrix} \frac{\partial f_1}{\partial x_1}(x_0) & \cdots & \frac{\partial f_1}{\partial x_n}(x_0) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1}(x_0) & \cdots & \frac{\partial f_n}{\partial x_n}(x_0) \end{pmatrix} \begin{pmatrix} x_1 - x_{0,1} \\ \vdots \\ x_n - x_{n,1} \end{pmatrix}$$



Recap: Nonlinear State Transition Model

- The actual state transition model is nonlinear of the form

$$x_k = f(x_{k-1}, u_k, v_k) \quad f: \mathbb{R}^n \times \mathbb{R}^m \times \mathbb{R}^p \rightarrow \mathbb{R}^n$$

- Using Taylor series expansion, we can approximate it as the linear system

$$x_k = F_k x_{k-1} + B_k u_k + G_k v_k$$

where $F_k \in \mathbb{R}^{n \times n}$ is the Jacobian of f with respect to x_{k-1} evaluated at the latest estimate $\hat{x}_{k-1 | k-1}$

$$F_k := \frac{\partial f}{\partial x_{k-1}}(\hat{x}_{k-1 | k-1}) = \begin{pmatrix} \frac{\partial f_1}{\partial x_1}(\hat{x}_{k-1 | k-1}) & \cdots & \frac{\partial f_1}{\partial x_n}(\hat{x}_{k-1 | k-1}) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1}(\hat{x}_{k-1 | k-1}) & \cdots & \frac{\partial f_n}{\partial x_n}(\hat{x}_{k-1 | k-1}) \end{pmatrix} \in \mathbb{R}^{n \times n}$$



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Note: we will not use the matrix B_k at all !



Recap: Nonlinear State Transition Model

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- Using Taylor series expansion, we can approximate it as the linear system

$$x_k = F_k x_{k-1} + B_k u_k + G_k v_k$$

where $G_k \in \mathbb{R}^{n \times p}$ is the Jacobian of f with respect to v_k evaluated at the latest estimate $\hat{x}_{k-1 | k-1}$

$$G_k := \frac{\partial f}{\partial v_k}(\hat{x}_{k-1 | k-1}) = \begin{pmatrix} \frac{\partial f_1}{\partial v_1}(\hat{x}_{k-1 | k-1}) & \cdots & \frac{\partial f_1}{\partial v_p}(\hat{x}_{k-1 | k-1}) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial v_1}(\hat{x}_{k-1 | k-1}) & \cdots & \frac{\partial f_n}{\partial v_p}(\hat{x}_{k-1 | k-1}) \end{pmatrix} \in \mathbb{R}^{n \times p}$$



Recap: Nonlinear Measurement Model

- The actual measurement model is nonlinear of the form

$$z_k = h(x_k, w_k) \quad h: \mathbb{R}^n \times \mathbb{R}^l \rightarrow \mathbb{R}^q$$

- Using Taylor series expansion, we can approximate it as the linear system

$$z_k = H_k x_k + L_k w_k$$

where $H_k \in \mathbb{R}^{q \times n}$ is the Jacobians of h with respect to x_k evaluated at the prediction $\hat{x}_{k|k-1}$

$$H_k := \frac{\partial h}{\partial x_k}(\hat{x}_{k|k-1}) = \begin{pmatrix} \frac{\partial h_1}{\partial x_1}(\hat{x}_{k|k-1}) & \cdots & \frac{\partial h_1}{\partial x_n}(\hat{x}_{k|k-1}) \\ \vdots & \ddots & \vdots \\ \frac{\partial h_q}{\partial x_1}(\hat{x}_{k|k-1}) & \cdots & \frac{\partial h_q}{\partial x_n}(\hat{x}_{k|k-1}) \end{pmatrix} \in \mathbb{R}^{q \times n}$$



Recap: Nonlinear Measurement Model

- The actual measurement model is nonlinear of the form

$$z_k = h(x_k, w_k) \quad h: \mathbb{R}^n \times \mathbb{R}^l \rightarrow \mathbb{R}^q$$

- Using Taylor series expansion, we can approximate it as the linear system

$$z_k = H_k x_k + L_k w_k$$

where $L_k \in \mathbb{R}^{q \times l}$ is the Jacobian of h with respect to w_k evaluated at the prediction $\hat{x}_{k|k-1}$

$$L_k := \frac{\partial h}{\partial w_k}(\hat{x}_{k|k-1}) = \begin{pmatrix} \frac{\partial h_1}{\partial w_1}(\hat{x}_{k|k-1}) & \cdots & \frac{\partial h_1}{\partial w_l}(\hat{x}_{k|k-1}) \\ \vdots & \ddots & \vdots \\ \frac{\partial h_q}{\partial w_1}(\hat{x}_{k|k-1}) & \cdots & \frac{\partial h_q}{\partial w_l}(\hat{x}_{k|k-1}) \end{pmatrix} \in \mathbb{R}^{q \times l}$$



Outline

- Recap last lectures
- **Extended Kalman Filter Algorithm**
- IMU Orientation Estimation



Prediction update: KF vs EKF

- Kalman Filter

- $\hat{x}_{k|k-1} = F_k \hat{x}_{k-1|k-1} + B_k u_k$
- $P_{k|k-1} = F_k P_{k-1|k-1} F_k^\top + Q_K$

- Extended Kalman Filter

- $\hat{x}_{k|k-1} = f(\hat{x}_{k-1|k-1}, u_k)$
- $P_{k|k-1} = F_k P_{k-1|k-1} F_k^\top + G_k Q_K G_k^\top$
- $F_k := \frac{\partial f}{\partial x_{k-1}}(\hat{x}_{k-1|k-1})$
- $G_k := \frac{\partial f}{\partial v_k}(\hat{x}_{k-1|k-1})$



Correction update: KF vs EKF

- Kalman Filter

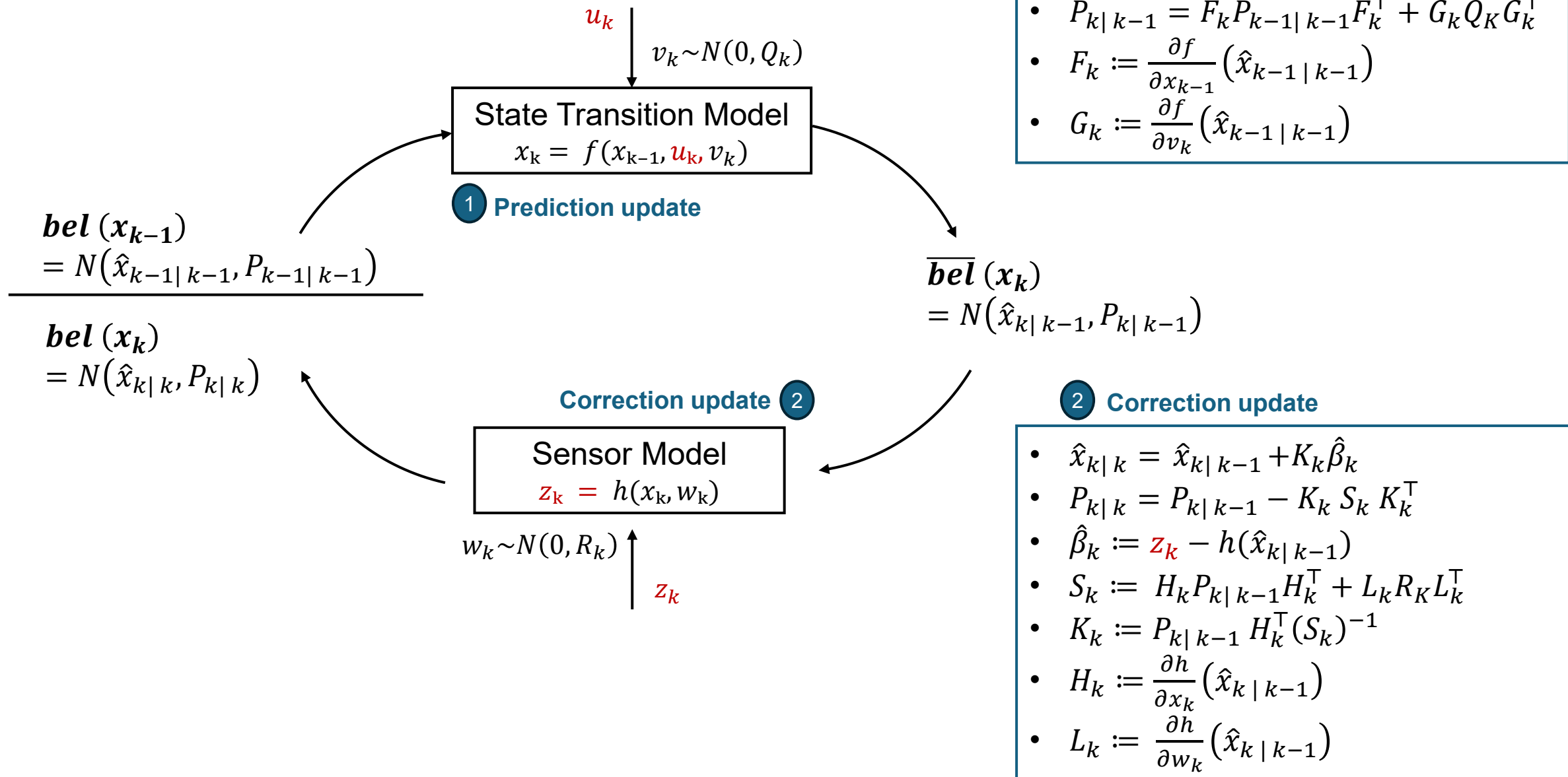
- $\hat{x}_{k|k} = \hat{x}_{k|k-1} + K_k \hat{\beta}_k$
- $P_{k|k} = P_{k|k-1} - K_k S_k K_k^\top$
- $\hat{\beta}_k := \mathbf{z}_k - H_k \hat{x}_{k|k-1}$
- $S_k := H_k P_{k|k-1} H_k^\top + R_K$
- $K_k := P_{k|k-1} H_k^\top (S_k)^{-1}$

- Extended Kalman Filter

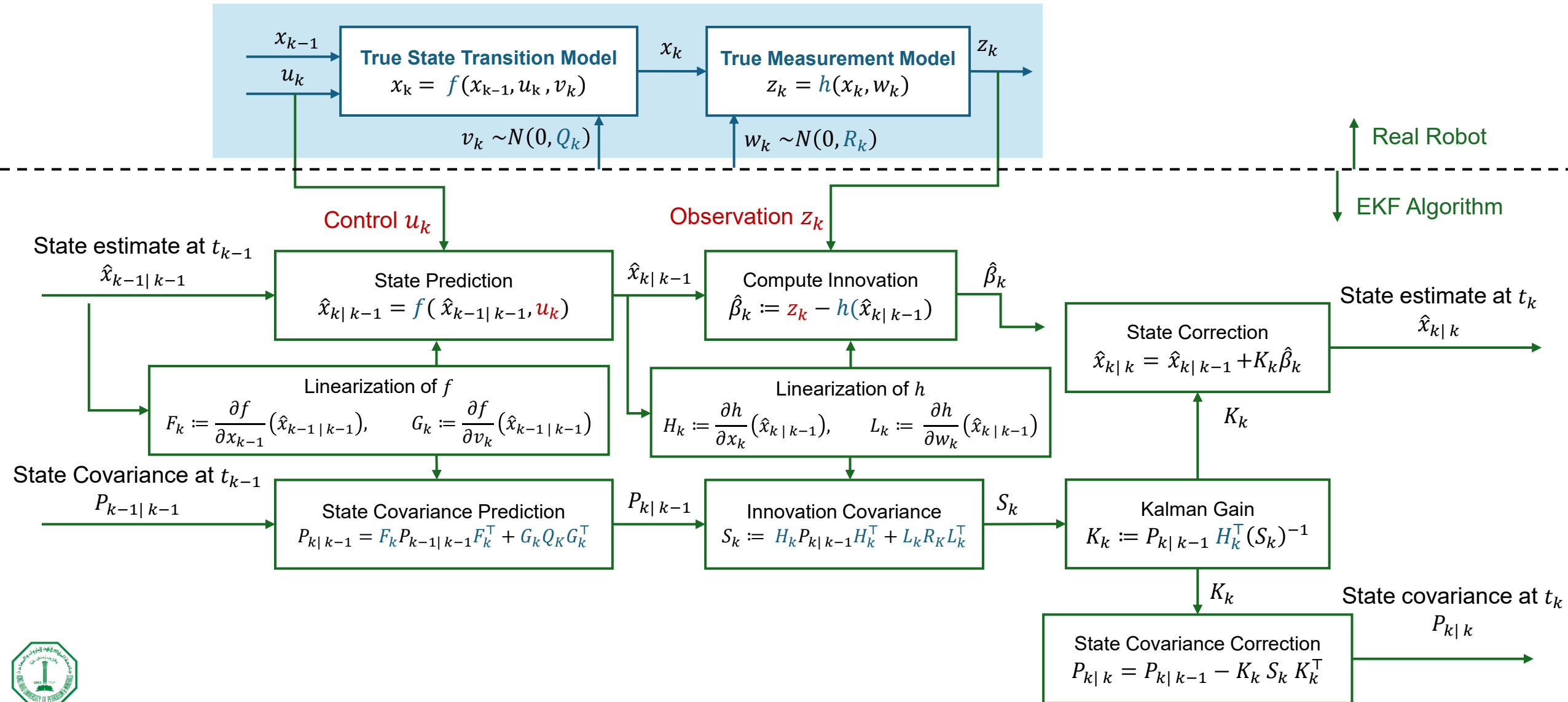
- $\hat{x}_{k|k} = \hat{x}_{k|k-1} + K_k \hat{\beta}_k$
- $P_{k|k} = P_{k|k-1} - K_k S_k K_k^\top$
- $\hat{\beta}_k := \mathbf{z}_k - h(\hat{x}_{k|k-1})$
- $S_k := H_k P_{k|k-1} H_k^\top + L_k R_K L_k^\top$
- $K_k := P_{k|k-1} H_k^\top (S_k)^{-1}$
- $H_k := \frac{\partial h}{\partial x_k}(\hat{x}_{k|k-1})$
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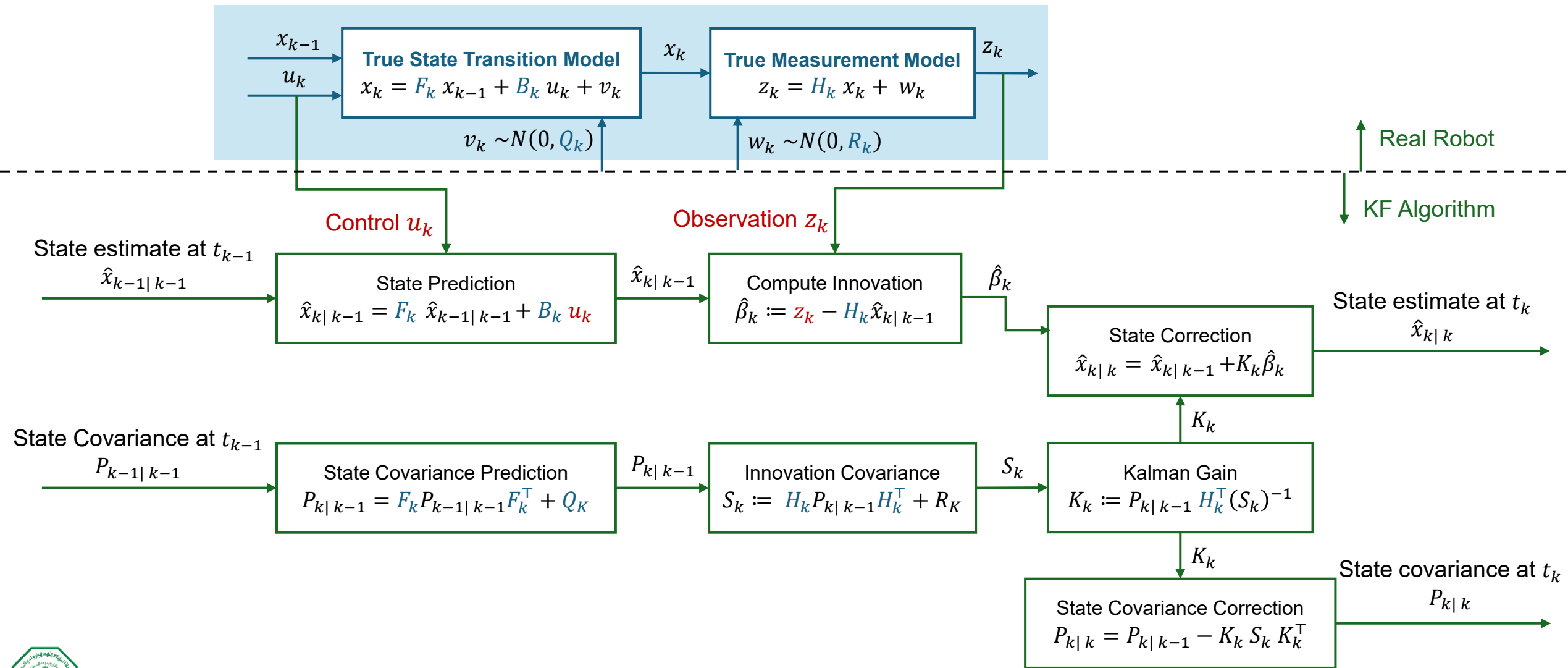
Extended Kalman Filter



EKF Block Diagram



Standard KF Block Diagram



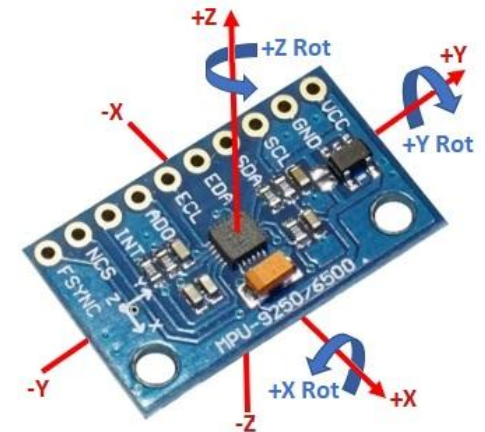
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- IMU Orientation Estimation



Problem formulation

- How to fuse the measurements of a 9DOF IMU to estimate the orientation of a robot $R \in SO(3)$?
 - Kinematic Model:
 - $\dot{R}_b^s = R_b^s [\omega]$
 - Gyroscope Model:
 - $\omega_m = \omega + b_g + \eta_g$
 - Accelerometer Model:
 - $a_m = R_s^b g + b_a + w_a$
 - Magnetometer Model:
 - $m_m = R_s^b \beta + b_m + w_m$



We assume the IMU is calibrated and non-accelerating.



Problem formulation

- How to fuse the measurements of a 9DOF IMU to estimate the orientation of a robot $R \in SO(3)$?
 - Kinematic Model:
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IMU Noise:

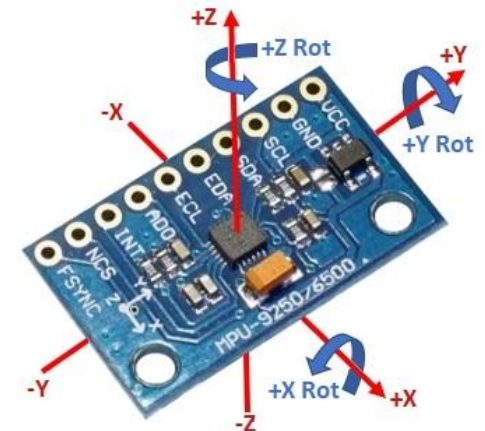
- $\eta_g \sim N(0, C_g)$
- $w_a \sim N(0, C_a)$
- $w_m \sim N(0, C_m)$

IMU Biases:

- $b_g, b_a, b_m \in \mathbb{R}^3$

Gravity and Environment Magnetic Field:

- $g = (0, 0, -9.81) \in \mathbb{R}^3$
- $\beta = (B_x, B_y, B_z) \in \mathbb{R}^3$



We assume the IMU is calibrated and non-accelerating.



Design Choices

- There are several choices that could be made leading to different Kalman Filter formulations:

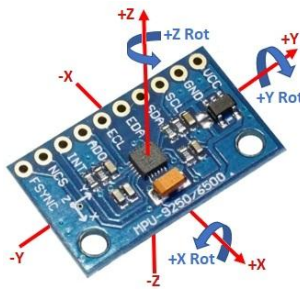
1. Orientation Parametrization:

- **Rotation Matrices** (orthonormality constraints, more complex to update)
- **Euler Angles** (intuitive but prone to gimbal lock and singularities)
- **Quaternions** (most common, avoids singularities and allows easy normalization)

2. Bias Handling:

- **Exclude bias** and assume external calibration or stationarity
- **Include gyroscope bias** in the state and model it as a random walk

3. Discretization Method



Random Walk

- A **random walk** is a process where a variable changes over time by adding small, random increments.
- Mathematically, you can express it as:

$$\dot{b}(t) = 0 + w(t), \quad w \sim N(0, Q)$$

- Or equivalently in discrete time as:

$$b_k = b_{k-1} + w_k$$

- This means the bias doesn't stay constant but also doesn't evolve in a predictable way, it just drifts slowly due to noise.



Why Use Random Walk for Bias Estimation?

- In many systems (e.g., inertial sensors like gyros or accelerometers), **biases are not truly constant**, but they:
 - Change slowly over time,
 - Cannot be measured directly,
 - Corrupt the measurements.
- Modeling them as random walks allows the Kalman filter to:
 - Adapt to changing biases,
 - Estimate them alongside the true state.
- The process noise covariance Q is a **tuning parameter** that controls how fast the bias is allowed to drift.



EKF Formulation 1

- Let's design an EKF based on Euler angles excluding biases
 - State vector:
 - (Roll, pitch, yaw) angles + Magnetic Field
 - $x = (\alpha, \beta) = (\phi, \theta, \psi, B_x, B_y, B_z) \in \mathbb{R}^6$
 - Kinematic Model:
 - $\dot{\alpha} = T(\alpha) \omega$
 - Unbiased Gyroscope Model:
 - $\omega_m = \omega + \eta_g$
 - Unbiased Accelerometer Model:
 - $a_m = R(\alpha)^\top g + w_a$
 - Unbiased Magnetometer Model:
 - $m_m = R(\alpha)^\top \beta + w_m$

$$T(\alpha) = \begin{pmatrix} 1 & s_\phi t_\theta & c_\phi t_\theta \\ 0 & c_\phi & -s_\phi \\ 0 & \frac{s_\phi}{c_\theta} & \frac{c_\phi}{c_\theta} \end{pmatrix}$$

$$R(\alpha) = \begin{pmatrix} c_\psi c_\theta & c_\psi s_\theta s_\phi - s_\psi c_\phi & c_\psi s_\theta c_\phi + s_\psi s_\phi \\ s_\psi c_\theta & s_\psi s_\theta s_\phi + c_\psi c_\phi & s_\psi s_\theta c_\phi - c_\psi s_\phi \\ -s_\theta & c_\theta s_\phi & c_\theta c_\phi \end{pmatrix}$$



EKF Formulation 1

- State Transition Model $\dot{x} = f(x, u, \eta)$:
 - $\begin{pmatrix} \dot{\alpha} \\ \dot{\beta} \end{pmatrix} = \begin{pmatrix} T(\alpha) [\omega_m + \eta_g] \\ \eta_\beta \end{pmatrix}$
- Discretized Model $x_k = f(x_{k-1}, u_k, \eta_k)$:
 - $\begin{pmatrix} \alpha_k \\ \beta_k \end{pmatrix} = \begin{pmatrix} \alpha_{k-1} + \Delta t T(\alpha_{k-1}) [\omega_{m,k} + \eta_{g,k}] \\ \beta_{k-1} + \eta_{\beta,k} \end{pmatrix}$
- Measurement Model $z_k = h(x_k) + w_k$:
 - $\begin{pmatrix} a_{m,k} \\ m_{m,k} \end{pmatrix} = \begin{pmatrix} R(\alpha_k)^\top g \\ R(\alpha_k)^\top \beta_k \end{pmatrix} + \begin{pmatrix} w_{a,k} \\ w_{m,k} \end{pmatrix}$

- $x = (\alpha, \beta) \in \mathbb{R}^6$
- $u = \omega_m \in \mathbb{R}^3$
- $z = (a_m, m_m) \in \mathbb{R}^6$

Noise Variables:

- $\eta_{g,k} \sim N(0, C_g)$
- $\eta_{\beta,k} \sim N(0, C_\beta)$
- $w_{a,k} \sim N(0, C_a)$
- $w_{m,k} \sim N(0, C_m)$

Question: How do we compute the Jacobians F_k, G_k, H_k, L_k ?

We choose here the Backward Euler Discretization method



EKF Formulation 2

- Now let's design a more practical EKF that includes biases:
 - State vector:
 - (Roll, pitch, yaw) angles + Magnetic Field
 - $x = (\alpha, b_g, b_a, b_m, \beta) \in \mathbb{R}^{15}$
 - Kinematic Model:
 - $\dot{\alpha} = T(\alpha) \omega$
 - Gyroscope Model:
 - $\omega_m = \omega + b_g + \eta_g$
 - Accelerometer Model:
 - $a_m = R(\alpha)^\top g + b_a + w_a$
 - Magnetometer Model:
 - $m_m = R(\alpha)^\top \beta + b_m + w_m$



EKF Formulation 2

- Discretized Model $x_k = f(x_{k-1}, u_k, \eta_k)$:

$$\bullet \begin{pmatrix} \alpha_k \\ b_{g,k} \\ b_{a,k} \\ b_{m,k} \\ \beta_k \end{pmatrix} = \begin{pmatrix} \alpha_{k-1} + \Delta t T(\alpha_{k-1}) [\omega_{m,k} - b_{g,k-1} + \eta_{g,k}] \\ b_{g,k-1} + \eta_{b_g,k} \\ b_{a,k-1} + \eta_{b_a,k} \\ b_{m,k-1} + \eta_{b_m,k} \\ \beta_{k-1} + \eta_{\beta,k} \end{pmatrix}$$

- Measurement Model $z_k = h(x_k) + w_k$:

$$\bullet \begin{pmatrix} a_{m,k} \\ m_{m,k} \end{pmatrix} = \begin{pmatrix} R(\alpha_k)^\top g + b_{a,k} \\ R(\alpha_k)^\top \beta_k + b_{m,k} \end{pmatrix} + \begin{pmatrix} w_{a,k} \\ w_{m,k} \end{pmatrix}$$

- $x = (\alpha, b_g, b_a, b_m, \beta) \in \mathbb{R}^{15}$
- $u = \omega_m \in \mathbb{R}^3$
- $z = (a_m, m_m) \in \mathbb{R}^6$

Noise Variables:

- $\eta_{g,k} \sim N(0, C_g)$
- $\eta_{\beta,k} \sim N(0, C_\beta)$
- $\eta_{b_g,k} \sim N(0, C_{b_g})$
- $\eta_{b_a,k} \sim N(0, C_{b_a})$
- $\eta_{b_m,k} \sim N(0, C_{b_m})$
- $w_{a,k} \sim N(0, C_a)$
- $w_{m,k} \sim N(0, C_m)$

Question: How do we compute the Jacobians F_k, G_k, H_k, L_k ?

